

REMARKS

Claims 11-21 are pending in this application. By this Preliminary Amendment, Applicants AMEND the abstract of the disclosure, CANCEL claims 1-10 and ADD new claims 11-21.

Applicants have attached hereto a Substitute Specification in order to make corrections of minor informalities contained in the originally filed specification. Applicants' undersigned representative hereby declares and states that the Substitute Specification filed concurrently herewith does not add any new matter whatsoever to the above-identified patent application. Accordingly, entry and consideration of the Substitute Specification are respectfully requested.

The changes to the specification have been made to correct minor informalities to facilitate examination of the present application.

Applicants respectfully submit that this application is in condition for allowance. Favorable consideration and prompt allowance are respectfully solicited.

Respectfully submitted,

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SURFACE ACOUSTIC WAVE BRANCHING FILTER

~~Technical~~ BACKGROUND OF THE INVENTION1. Field of the Invention

[0001] — The present invention relates to a surface acoustic wave branching filter ~~using~~ including first and second surface acoustic filters having different passbands and more particularly, the present invention relates to a surface acoustic wave branching filter of a ladder-type circuit structure having pluralities of a plurality of series-arm resonators and a plurality of parallel-arm resonators.

~~Background Art~~2. Description of the Related Art

[0002] — Up to now, various surface acoustic wave branching filters using a surface acoustic wave filter of a ladder-type circuit structure having series-arm resonators and parallel-arm resonators have been proposed.

[0003] — For example, ~~in the following~~ Japanese Unexamined Patent Document 1, Application Publication No. 2000-315936 discloses a surface acoustic wave branching filter, as shown in Fig. 12 is disclosed. Here, a first surface acoustic wave filter F_1 for relatively low frequencies and a second surface acoustic wave filter F_2 for relatively high frequencies are connected to an antenna-side common terminal T_0 . The first surface acoustic wave filter F_1 includes a series-arm resonator

R_{S0} and a parallel-arm resonator R_P , and the second surface acoustic wave filter F_2 includes a parallel-arm resonator R_{P0} and a series-arm resonator R_S .

[0004] ——— In the first surface acoustic wave filter F_1 , a resonator ~~close~~that is closest to the common antenna terminal T_0 is the series-arm resonator R_{S0} and, in the second surface acoustic wave filter F_2 , a ~~resonance close to the resonator~~that is closest to the common antenna terminal T_0 is the parallel-arm resonator R_{P0} .

[0005] ——— Furthermore, a phase rotation line S is sandwiched between the second surface acoustic wave filter F_2 and the common antenna terminal T_0 .

[0006] ——— ~~On the other hand, in the following Patent Document 2, Japanese Unexamined Patent Application Publication No. 10-93382 discloses a surface acoustic wave filter of a ladder-type circuit structure, as shown in Fig. 13 is disclosed.~~ Here, series-arm resonators R_{S1} and R_{S2} are connected in series in a series arm between an input terminal and an output terminal. Furthermore, a parallel-arm resonator R_{P1} is disposed in a parallel arm connected between the input terminal and the series-arm resonator R_{S1} . ~~Furthermore, a~~A parallel-arm resonator R_{P2} is disposed in a parallel arm, one end of which is connected between the series-arm resonators R_{S1} and R_{S2} . Moreover, a parallel-arm resonator R_{P3} is disposed in a parallel arm between the series-arm resonator R_{P2} R_{S2} and the output terminal.

[0007] ——— In this surface acoustic wave filter, the three parallel-arm resonators R_{P1} to R_{P3} are commonly connected to a

common terminal 51 on a surface acoustic wave chip. Then, the common terminal 51 and the ground terminal of a package are connected by a bonding wire having an inductance L_E .

[0008] ~~On the other hand, in the following Patent Document 3, it is described that, in~~Japanese Unexamined Patent Application Publication No. 5-183380 describes a surface acoustic wave filter of a ladder-type circuit structure,~~wherein the best capacitance ratio is 1/2 between a parallel-arm resonator disposed at an end portion and a parallel-arm resonator connected in a parallel arm sandwiched between series-arm resonators is 1/2.~~

[0009] ~~Moreover, in the following~~Japanese Unexamined Patent Document 4, Application Publication No. 2001-298348 discloses a surface acoustic wave branching filter, as shown in Fig. 14 is disclosed. As shown in Fig. 14, in a surface acoustic wave branching filter 70, a first surface acoustic wave filter 61 for relatively low frequencies and a second surface acoustic wave filter 62 for relatively high frequencies are connected to a common terminal 71 on the antenna side in a surface acoustic wave branching filter 70.
The surface acoustic wave filters 61 and 62 are surface acoustic wave filters of a ladder-type circuit structure having series-arm resonators S1 to S3 and parallel-arm resonators P1 to P6, respectively.

~~Patent Document 1:~~In a surface acoustic wave branching filter described inJapanese Unexamined Patent Application Publication No. 2000-315936

~~Patent Document 2:~~Japanese Unexamined Patent Application

~~Publication No. 10-93382~~

~~Patent Document 3: Japanese Unexamined Patent Application~~

~~Publication No. 5-183380~~

~~Patent Document 4: Japanese Unexamined Patent Application~~

~~Publication No. 2001-298348~~

~~Disclosure of Invention~~

~~[0010]~~ ——— In a surface acoustic wave branching filter described in Patent Document 4, the series-arm resonator R_{S0} is connected to a first stage of the first surface acoustic wave filter F_1 for relatively low frequencies, and the above-described phase rotation line S is connected to the second surface acoustic wave filter F_2 .

~~[0011]~~ ——— In recent years, the reduction in size has also been strongly required in surface acoustic wave branching filters. Accordingly, when the phase rotation line S is ~~constituted~~provided in a package, it has been difficult to ensure a sufficient line length for fully rotating the phase. Furthermore, the longer the line length of the phase rotation line S , the larger the resistance of the line. Accordingly, there has been a problem in that the loss of the surface acoustic wave branching filters increases.

~~[0012]~~ ——— On the other hand, when the line length of the phase rotation line S is reduced, the amount of phase rotation becomes small, the impedance matching of the surface acoustic wave filter F_2 deviates from a reference impedance of $50\ \Omega$, the loss in the band increases, and there was a ~~fear~~concern that isolation characteristics might deteriorate.

~~[0013]~~ ——— In the surface acoustic wave filter described in

the above-described Japanese Unexamined Patent Document
Application Publication No. 10-93382, it is stated that the
amount of attenuation can be improved by commonly connecting
the ground-side terminals of the parallel-arm resonators R_{P1} to
 R_{P3} . However, ~~in Patent Document 2,~~ only a technique for
improving the amount of attenuation of a surface acoustic wave
filter is disclosed, and, ~~in Patent Document 2,~~ nothing about
the ~~concrete~~specific structure of series-arm resonators and
parallel-arm resonators in a surface acoustic wave branching
filter is described.

[0014] ~~—~~Furthermore, in Japanese Unexamined Patent
~~Document 3~~Application Publication No. 5-183380, in the surface
acoustic wave filter of a ladder-type circuit structure,
although the capacitance ratio between a parallel-arm
resonator disposed at an end portion and a parallel-arm
resonator in a parallel arm disposed between series-arm
resonators is described, it is only described to make the
capacitance ratio of the parallel-arm resonators a fixed value.
That is, nothing is described concerning a desirable structure
of the series-arm resonators and the parallel-arm resonators
in surface acoustic wave branching filters using a plurality
of surface acoustic wave filters.

[0015] ~~—~~In the surface acoustic wave branching filter
described in the ~~above Patent Document 4~~Japanese Unexamined
Patent Application Publication No. 2001-298348, the surface
acoustic wave branching filter 70 using the surface acoustic
wave filters 61 and 62 ~~in which a resonator closest to the~~
~~common terminal 71 is~~has the parallel-arm resonator S_1 that is

closest to the common terminal 71. However, in the surface acoustic wave branching filter 70, a desirable structure of each of the series-arm resonators S1 to S3 and parallel-arm resonators P1 to P6, phase delay circuits, etc., are not particularly specifically mentioned.

~~It is an object of the present invention~~

SUMMARY OF THE INVENTION

[0016] In order to overcome the problems described above, preferred embodiments of the present invention provide a structure ~~surface acoustic wave branching filter capable of~~ being able to be reduced in size without having isolation characteristics deteriorated and having the loss increased in ~~a surface acoustic wave branching filter in which a first~~ surface acoustic wave filter having a relatively low passband and a second surface acoustic wave filter having a relatively high passband are connected to a common terminal on the antenna side and each surface acoustic wave filter ~~is composed of a~~ includes a ladder-type surface acoustic wave filter.

[0017] ~~In the present invention~~ In a preferred embodiment, a surface acoustic wave branching filter includes a first surface acoustic wave filter having a relatively low passband, a second surface acoustic wave filter having a relatively high passband, and a first common terminal to which ~~one first~~ ends of the first and second surface acoustic wave filters are connected and which is, wherein the first common terminal is connected to an antenna. In the surface acoustic wave branching filter, the first surface acoustic wave filter is a surface acoustic wave filter of a ladder-type

circuit structure having a plurality of parallel-arm resonators and a plurality of series-arm resonators.

[0018] ~~Out of the pluralities~~ A resonator, among the plurality of series-arm resonators and the plurality of parallel-arm resonators, ~~a resonator being the~~ that is closest to the first common terminal is a parallel-arm resonator and the capacitance of the parallel-arm resonator ~~being the~~ that is closest to the first common terminal is less than $1/2$ of the capacitance of ~~a the other~~ parallel-arm resonator, ~~different from the parallel arm resonator,~~ sandwiched between the series-arm resonators.

[0019] ~~In a particular aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the capacitance of the parallel-arm resonator ~~being the~~ that is closest to the first common terminal is in the range of about $1/40$ to about $1/5$ of the capacitance of the other parallel-arm resonator sandwiched between different series-arm resonators.

[0020] ~~In another particular aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the surface acoustic wave branching filter further includes a second common terminal to which one end of a parallel-arm resonator ~~being the~~ that is closest to the first common terminal and one end of the other parallel-arm resonator are connected, and an inductance element is added between the second common terminal and the ground potential.

[0021] ~~In another particular aspect~~ preferred embodiment of a surface acoustic wave branching filter of the

present invention, the surface acoustic wave branching filter further includes a package material housing the first and second surface acoustic wave filters, ~~wherein~~ and the second common terminal is included in the package material.

[0022] ———In another particular ~~aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the resonance frequency of the parallel-arm resonator ~~being the~~ that is closest to the first common terminal is substantially the same as the resonance frequency of the other parallel-arm resonator.

[0023] ———In another particular ~~aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the surface acoustic wave branching filter further ~~comprises~~ includes a phase adjustment element ~~inserted~~ located between the second surface acoustic wave filter and the first common terminal.

[0024] ———In another particular ~~aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the amount of phase delay of the phase adjustment element is less than 90 degrees from the central frequency of the first surface acoustic wave filter and, when seen from the side of the first common terminal, at least 50% of the passband of the second surface acoustic wave filter is inductive.

[0025] ———In another particular ~~aspect~~ preferred embodiment of a surface acoustic wave branching filter of the present invention, the phase adjustment element is a stripline.

[0026] ———In another particular ~~aspect~~ preferred

embodiment of a surface acoustic wave branching filter of the present invention, the phase adjustment element includes a capacitance element and a second inductance element.

[0027] —In another particular aspect, preferred embodiment of a surface acoustic wave branching filter of the present invention, when seen from the first common terminal, at least 50% of the passband of the second surface acoustic wave filter is inductive.

[0028] —In a surface acoustic wave branching filter of preferred embodiments of the present invention, one first ends of a first surface acoustic wave filter having a relatively low passband and a second surface acoustic wave filter having a relatively high passband are connected to a first common terminal connected to an antenna side; in. In the surface acoustic wave branching filter in which the first surface acoustic wave filter is composed of includes a surface acoustic wave filter of a ladder-type circuit structure, out of pluralities a resonator, from a plurality of series-arm resonators and a plurality of parallel-arm resonators of the first surface acoustic wave filter, a resonator being the, which is closest to the first common terminal is a parallel-arm resonator; and the. The capacitance of the parallel-arm resonator being the that is closest to the first common terminal is less than about 1/2 of the capacitance of the other parallel-arm resonator sandwiched between the series-arm resonators different from the parallel-arm resonator.

Therefore, while deterioration of the ~~of the~~ insertion loss is ~~suppressed~~ reduced, isolation characteristics can be improved.

In particular, when the ~~above~~-capacitance ratio is in the range of about 1/40 to about 1/5, deterioration of the insertion loss is ~~more-suppressed~~ further reduced and simultaneously isolation characteristics can be effectively improved.

[0029] ~~—~~One end of the parallel-arm resonator ~~being the~~ that is closest to the first common terminal and one end of the other parallel-arm resonator are connected to a second common terminal, and, when an inductance element is connected between the second common terminal and the ground potential, even if the capacitance of the parallel-arm resonator is reduced, isolation characteristics can be more effectively improved.

[0030] ~~—~~Furthermore, when the second common terminal is included in a package, the ~~above~~-inductance element can be ~~constituted~~ provided in the package and the surface acoustic wave filter can be reduced in size.

[0031] ~~—~~When the resonance frequency of the parallel-arm resonator ~~being the~~ that is closest to the first common terminal is substantially the same as the resonance frequency of the other parallel-arm resonators, isolation characteristics can be effectively improved without ~~having~~ causing insertion loss due to the difference of characteristics of the parallel-arm resonators ~~caused~~.

[0032] ~~—~~When a phase adjustment element is ~~inserted~~ located between the second surface acoustic wave filter and the first common terminal, the loss at the first common terminal on the antenna side can be effectively reduced

by the phase adjustment element.

[0033] ———When the amount of phase delay of the phase adjustment element is less than about 90 degrees from the central frequency of the first surface acoustic wave filter and, when seen from the side of the first common terminal, at least 50% of the passband of the second surface acoustic wave filter is inductive, the DPX coupling loss at the common terminal on the antenna side can be effectively reduced.

[0034] ———When the phase adjustment element ~~is composed of~~ includes a stripline, the stripline can be easily formed in the package and the loss can be reduced without preventing the reduction in size of a surface acoustic wave branching filter ~~in size~~.

[0035] ———When the phase adjustment element is a phase adjustment circuit having a capacitance element and a second inductance element, the DPX coupling loss at the common terminal on the antenna side can be ~~more~~ further reduced.

[0036] ———When seen from the side of the first common terminal, if at least 50% of the passband of the second surface acoustic wave filter is inductive, the DPX coupling loss at the common terminal on the antenna side can be effectively reduced.

~~Brief Description of the Drawings~~

[0037] ———Other features, elements, steps, advantages and characteristics of the present invention will become more apparent from the following detailed description of preferred embodiments thereof with reference to the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0038] Fig. 1 shows the circuit structure of a surface acoustic wave branching filter according to onea preferred embodiment of the present invention.

[0039] ———Fig. 2 is a schematic top view showing the electrode structure of a surface acoustic wave resonator used as a series-arm resonator or parallel-arm resonator in thea preferred embodiment of the present invention.

[0040] ———Fig. 3 is a schematic sectional front view showing the physical structure of the surface acoustic wave branching filter of thea preferred embodiment of the present invention.

[0041] ———Fig. 4 shows the change of isolation when the capacitance ratio of the parallel-arm resonator in the surface acoustic wave branching filter of the first preferred embodiment is changed.

[0042] ———Fig. 5 shows isolation characteristics when the parallel-arm resonator ~~being the~~ that is closest to a first common terminal on the antenna side is not included and when the capacitance ratio of the parallel-arm resonator is approximately 1/20 and approximately 1/10.

[0043] ———Fig. 6 shows the ~~relation~~ relationship between the capacitance ratio and the insertion loss of a parallel-arm resonator.

[0044] ———Fig. 7 shows frequency characteristics of the amount of attenuation when a parallel-arm resonator ~~being the~~ that is closest to a first common terminal in a surface acoustic wave filter is not included and when the capacitive

ratio of a parallel-arm resonator is approximately 1/20 and approximately 1/10.

[0045] ——— Fig. 8 shows the ~~relation~~relationship between the capacitance ratio of a parallel-arm resonator and the insertion loss of a transmission side surface acoustic wave filter.

[0046] ——— Fig. 9 shows frequency characteristics of the amount of attenuation of a reception side surface acoustic wave filter when the parallel-arm resonator as a resonator ~~being the~~that is closest to the first common terminal in a first surface acoustic wave filter is not included and when the capacitance ratio of the parallel-arm resonator is approximately 1/20 and approximately 1/10.

[0047] ——— Fig. 10 shows the change of admittance on an admittance Smith chart when the phase is capacitive in the case where the resonator ~~being the~~that is closest to the first common terminal on the antenna side is a parallel-arm resonator.

[0048] ——— Fig. 11 shows the change of impedance on an impedance Smith chart when the series-arm resonator is capacitive in the case where the resonator ~~being the~~that is closest to the first common terminal on the antenna side is a series-arm resonator.

[0049] ——— Fig. 12 is a circuit diagram showing one example of related surface acoustic wave branching ~~filters~~filters.

[0050] ——— Fig. 13 is a circuit diagram showing one example of related surface acoustic wave branching ~~filters~~filters.

[0051] ——— Fig. 14 is a circuit diagram showing another

example of related surface acoustic wave branching
~~filters~~filters.

~~Reference Numerals~~

- ~~1 surface acoustic wave branching filter~~
- ~~2 antenna terminal~~
- ~~3 low pass filter~~
- ~~4 first common terminal~~
- ~~5 transmission side surface acoustic wave filter (first surface acoustic wave filter)~~
- ~~5A transmission side surface acoustic wave filter chip~~
- ~~6 reception side surface acoustic wave filter (second surface acoustic wave filter)~~
- ~~6A reception side surface acoustic wave filter chip~~
- ~~7 second common terminal~~
- ~~9 phase adjustment element~~
- ~~11 surface acoustic wave resonator~~
- ~~12 comb electrode~~
- ~~13 and 14 reflectors~~
- ~~15 case material~~
- ~~16 lid~~
- ~~17 package~~
- ~~18 metal bump~~
- ~~19, 20, and 21 via hole electrodes~~
- ~~22 and 23 striplines~~
- ~~24 to 26 via hole electrodes~~
- ~~ANT antenna~~
- ~~Z inductance element~~

~~Best Mode for Carrying Out the Invention~~

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

[0052] Hereinafter, the present invention is made clear by describing ~~concrete~~preferred embodiments of the present invention with reference to the drawings.

[0053] —Fig. 1 shows the circuit structure of a surface acoustic wave branching filter according to a first preferred embodiment of the present invention.

[0054] —In the surface acoustic wave branching filter of the present preferred embodiment, the passband on the transmission side is about 824 MHz to about 849 MHz and the passband on the reception side is about 869 to MHz to about 894 MHz.

[0055] —A surface acoustic wave branching filter 1 includes an ANT terminal 2 belonging to an antenna ANT. One end of a low-pass filter 3 is connected to the ANT terminal 2 and the other end of the low-pass filter 3 is connected to a first common terminal 4. That is, the first common terminal 4 is connected to the antenna ANT through the low-pass filter 3.

[0056] —A transmission side surface acoustic wave filter 5 as a first surface acoustic wave filter having a relatively low passband and a reception side surface acoustic wave filter 6 as a second surface acoustic wave filter having a relatively high passband are connected to the first common terminal 4.

[0057] —Each of the transmission side surface acoustic wave filter 5 and the reception side surface acoustic wave filter 6 is a surface acoustic wave filter of a ladder-type circuit structure having a plurality of series-arm resonators

and a plurality of parallel-arm resonators.

[0058] ——— Fig. 2 is a schematic top view showing the electrode structure of one surface acoustic wave resonator used as a parallel resonator or a series resonator in the surface acoustic wave filters 5 and 6. A surface acoustic wave resonator 11 includes a comb electrode 12 and reflectors 13 and 14 disposed on both sides in the surface acoustic wave propagation direction of the comb electrode 12. Moreover, in each of the series resonators and parallel resonators, the number, pitch, etc., of electrode fingers of the comb electrodes are properly selected in accordance with its capacitance and frequency.

[0059] ——— The transmission side surface acoustic wave filter 5 includes series-arm resonators T2, T3, T5, T6, T8, and T9 and parallel-arm resonators T1, T4, and T7. In the transmission side surface acoustic wave filter 5, a resonator ~~being the~~ that is closest to the first common terminal 4 is the parallel-arm resonator T1. The parallel-arm resonator T4 is included in a parallel arm, one end of which is connected between the series-arm resonators T3 and T5. Furthermore, the parallel-arm resonator T7 is disposed in a parallel arm, one end of which is connected between the series-arm resonators T6 and T8.

[0060] ——— The ground-side terminal of the parallel-arm resonators T1, T4, and T7 is commonly connected to a second common terminal 7 included in a package to be described later. Furthermore, an inductance element Z is connected between the second common terminal 7 and the ground potential.

[0061] ~~On the other hand, the~~ The reception side surface acoustic wave filter 6 as the second surface acoustic wave filter includes parallel-arm resonators R1, R4, and R7 and series-arm resonators R2, R3, R5, and R6. Out of these resonators, the parallel-arm resonator R1 is the closest resonator to the first common terminal 4. The parallel-arm resonator R4 is included in a parallel arm, one end of which is connected between the series-arm resonators R3 and R5, and the parallel-arm resonator R7 is disposed in a parallel arm, one end of which is connected between the series-arm resonator R6 and an a reception-side output terminal.

[0062] ~~Moreover,~~ a phase adjustment element 9 is disposed between the reception side surface acoustic wave filter 6 and the first common terminal 4.

[0063] ~~Fig. 3 is a schematic sectional front view showing the physical structure of the surface acoustic wave branching filter of the present preferred embodiment. The surface acoustic wave branching filter 1 includes a package 17 preferably having a case material 15 and a lid 16. The case material 15 is preferably made up of a case material 15 and a lid 16. The case material 15 is composed of an insulating eeramies such as aluminum, etc. ceramic such as alumina, for example, or an insulating material such as synthetic resin, etc. for example. The lid 16 is composed preferably made of an appropriate material such as a conductive material of metal, etc. for example, or an insulating material such as alumina, etc. for example.~~

[0064] ~~The case material 15 includes a concave portion~~

15a which is open upward, ~~and~~ and houses a transmission side surface acoustic wave filter chip 5A constituting the transmission side surface acoustic wave filter 5 and a reception side surface acoustic wave filter chip 6A constituting the reception side surface acoustic wave filter 6 ~~are housed in the concave portion 15a~~. The surface acoustic wave filter chips 5A and 6A are mounted on the case material 15 by a flip-chip bonding method. Fig. 3 shows the surface acoustic wave filter chips 5A and 6A joined to the bottom surface of the concave portion 15a by metal bumps 18, shown schematically ~~shown~~. In practice, the electrodes of the surface acoustic wave filter chips 5A and 6A are electrically connected to the electrode lands formed-disposed on the bottom surface of the concave portion ~~45-15a~~ 15a of the case material 15 by the metal bumps 18.

[0065] ~~—~~ Furthermore, via-hole electrodes 19 and 20 are formed in the case material 15. A phase adjustment element 9 ~~composed of~~ preferably including striplines 22 and 23 connected by a via-hole electrode 21 is ~~constituted~~ arranged between the via-hole electrodes 19 and 20.

[0066] ~~— On the other hand, via~~ Via-holes electrodes 24 and 25 are disposed under the transmission side surface acoustic wave filter chip 5A in the case material 15. The upper end of the via-hole electrodes 24 and 25 reach the bottom surface of the concave portion 15a of the case material 15, and the upper ~~end is~~ ends are connected to the parallel-arm resonators T4 and T1 shown in Fig. 1. The lower ~~end~~ ends of the via-hole electrodes 24 and 25 ~~is~~ are connected to the

second common terminal 7. The via-hole electrode (not shown in Fig. 3) connected to the ground-side terminal of the parallel-arm resonator T7 shown in Fig. 1 is also connected to the second common terminal 7.

[0067] —The second common terminal 7 is embedded in the case material 15, and the upper end of a via-hole electrode 26 is connected to the lower surface of the second common terminal 7. The lower end of the via-hole electrode 26 reaches the lower surface of the case material 15 and is connected to a ground electrode (not illustrated) ~~formed~~disposed on the lower surface of the case material 15.

[0068] —In the ~~present~~present preferred embodiment, the surface acoustic wave filter chips 5A and 6A are ~~constituted~~constructed in such a way that a surface acoustic wave resonator and electrodes constituting connection electrodes are ~~formed~~provided on a LiTaO₃ substrate preferably by using an electrode material having aluminum as a main component.

[0069] —Furthermore, the ~~above~~phase adjustment striplines 22 and ~~23~~23 preferably have a characteristic impedance of about 50 Ω , and the amount of phase shift is set in such a way that the phase is rotated by about 75 degrees at 836.5 MHz as the center frequency of the passband of the transmission side surface acoustic wave filter 5, for example.

[0070] —~~The~~One of the unique characteristics of the surface acoustic wave branching filter of the present preferred embodiment ~~is characterized in that~~, in the transmission side surface acoustic wave filter 5 having a

relatively low passband as described above, the parallel-arm resonator ~~thethat~~ is closest to the first common terminal 4, that is, the parallel-arm resonator ~~thethat~~ is closest to the antenna side is the parallel-arm resonator T1 ~~and the~~. The capacitance of the parallel-arm resonator T1 is preferably less than about 1/10 of the capacitance of the other parallel-arm resonators T4 and T7, ~~different from the parallel-arm resonator T1,~~ sandwiched between the series-arm resonators. In such a way, leakage of a signal to the reception side surface acoustic wave filter 6 from the transmission side surface acoustic wave filter 5 ~~can be suppressed~~ is reduced and minimized. That is, isolation characteristics can be improved. This is described with reference to Figs. 4 to 9.

[0071] —In the present preferred embodiment, the number of pairs of electrode fingers, the cross width of electrode fingers, the wavelength, and the number of electrode fingers of reflectors of each resonator used in the transmission side surface acoustic wave filter 5 and the reception side surface acoustic wave filter 6 are as shown in Table 1 and Table 2.

Table 1

No. of resonator	Number of pairs	Cross width	Wavelength	Number of electrode fingers of reflector
T 1	5 0	2 0	4. 8 9 2	1 5
T 2	1 6 4	1 1 0	4. 6 5 6	1 5
T 3	1 6 4	1 1 0	4. 6 6 7	1 5
T 4	8 0	1 2 5	4. 8 9 2	1 5
T 5	1 1 2	1 0 2	4. 6 6 2	1 5
T 6	1 1 2	1 0 2	4. 6 6 2	1 5
T 7	8 0	1 2 5	4. 8 9 2	1 5
T 8	1 1 2	2 0 0	4. 6 7 3	1 5
T 9	1 6 3	1 3 5	4. 6 9 4	1 5

Table 2

No. of resonator	Number of pairs	Cross width	Wavelength	Number of electrode fingers of reflector
R 1	1 2 5	6 4	4. 5 7 5	1 5
R 2	1 1 5	1 2 6	4. 3 6 8	1 5
R 3	1 1 5	3 9. 4	4. 3 6 8	1 5
R 4	1 2 5	2 0 3. 5	4. 5 6 9	1 5
R 5	1 1 5	3 9. 4	4. 3 6 8	1 5
R 6	1 1 5	1 2 6	4. 3 6 8	1 5
R 7	1 1 2	7 2	4. 5 7 5	1 5

[0072] —Furthermore, since the result shown in Figs. 4 to 9 was obtained by properly modifying the structure (construction) of the resonators used in the surface acoustic wave branching filter of the above-described preferred embodiment, and the case in which the capacitance ratio is about 1/10 corresponds to the present embodiment.

[0073] —Fig. 4 shows the change of isolation when the capacitance ratio between the parallel-arm resonator T1 and the parallel-arm resonators T4 and T7 is changed. Fig. 5 shows isolation characteristics when the parallel-arm resonator T1 is not connected and when the ~~above~~ capacitance ratio of the parallel-arm resonator T1 is about 1/20 and about 1/10 (representing the present preferred embodiment).

Furthermore, Fig. 6 shows the ~~relation~~relationship between the capacitance ratio and the insertion loss of the transmission side surface acoustic wave filter. Fig. 7 shows insertion loss characteristics of each transmission side surface acoustic wave filter when the parallel-arm resonator T1 is not connected and when the capacitance ratio of the parallel-arm resonator T1 is about 1/20 and about 1/10 in the same way as

in Fig. 5.

[0074] —Furthermore, Fig. 8 shows the insertion loss of a reception side surface elastic-wave-filter acoustic wave filter relative to the capacitance ratio. Fig. 9 shows the insertion loss of each reception side surface acoustic wave filter in the case when the parallel-arm resonator T1 is not connected and when the capacitance ratio of the parallel-arm resonator T1 is about $1/20$ and about $1/10$. Moreover, the inner attenuation value to frequency characteristics shown in Fig. 9 are magnified in accordance with the right-hand scale of the perpendicular axis.

[0075] —Moreover, in Fig. 7, the inner attenuation value to frequency characteristics are magnified in accordance with the right-hand scale of the vertical axis.

[0076] —As is clearly understood from Fig. 5, leakage from the transmission side surface acoustic wave filter 5 to the reception side surface acoustic wave filter 6 is ~~suppressed~~ reduced and isolation characteristics can be improved by ~~having~~ providing the parallel-arm resonator T1 ~~provided when~~ compared with the case where the parallel-arm resonator T1 is not provided, ~~that~~. That is, the case where the resonator ~~the~~ that is closest to the first common terminal 1 is the series-arm resonator T2 in the transmission side surface acoustic wave filter 5. Furthermore, as clearly understood from Fig. 4, isolation characteristics can be improved particularly in the vicinity where the capacitance ratio is about $1/10$. That is, when a resonator of the transmission side surface acoustic wave filter 5 which is the

closest to the first common terminal 4 on the antenna side is the parallel-arm resonator T1, it is understood that isolation characteristics can be improved in comparison with the case where the resonator which is ~~the~~ closest to the common terminal 4 is a series-arm resonator.

[0077] ———Accordingly, in the surface acoustic wave filter circuit of a ladder-type circuit structure, up to now, ~~although it is stated that the most appropriate capacitance ratio is 1/2~~ as described in Japanese Unexamined Patent Document 3, when Application Publication No. 5-183380, the most appropriate capacitance ratio is 1/2. When the change of isolation characteristics in Fig. 4 is considered, it is understood that the capacitance ratio of less than 1/2 is desirable in the surface acoustic wave branching filter having the first and second surface acoustic wave filters connected therein. ~~That is, it~~ It is understood that, by making the capacitance ratio less than 1/2, a surface acoustic wave branching filter in which improved isolation characteristics ~~are improved~~ can be provided in comparison with the case where a surface acoustic wave filter having a capacitance ratio of 1/2 is used.

[0078] ———On the other hand, as is understood from Fig. 4, when the capacitance ratio is less than about 1/40 or exceeds about 1/5, isolation characteristics become equivalent to the case where the parallel-arm resonator is not connected (capacitance ratio = 0). Accordingly, it is desirable to make the capacitance ratio in the range of about 1/40 or higher and about 1/5 or lower.

[0079] —As is clearly understood from Figs. 5, 6, 8, and 9, there is a tendency that the higher the capacitance ratio becomes, the larger the loss of the transmission side surface acoustic wave filter 5 and the loss of the reception side surface acoustic wave filter 6 become. However, as is clearly understood from Figs. 6 to 9, when the capacitance ratio is about 1/5 or less, the loss in the transmission side surface acoustic wave filter 5 and the reception side surface acoustic wave filter 6 is relatively small.

[0080] —Accordingly, ~~more preferably~~, when the capacitance ratio is in the range of about 1/40 to about 1/5, deterioration of the insertion loss is ~~suppressed~~ reduced and simultaneously isolation characteristics can be improved.

[0081] —Furthermore, in the present preferred embodiment, the grounding side terminal of the parallel-arm resonator T1 which is ~~the~~ closest to the first common terminal 4 and the grounding side terminal of the other parallel-arm resonators T4 and T7 included in the surface acoustic wave filter chip 5A are commonly connected to the second common terminal 7. Then, the second common terminal 7 is connected to the ground potential through the inductance element Z. Accordingly, since the inductance element Z is added at the portion where the parallel-arm resonator T1 is connected to the other parallel-arm resonators T4 and T7 through the common terminal 7, even if the capacitance of the parallel-arm resonator T1 is small, isolation characteristics can be effectively improved.

[0082] —~~Furthermore, preferably, the~~ The resonance frequency of the parallel-arm resonator T1 is preferably made

the same as the resonance frequency of the other parallel-arm resonators T4 and T7. In that case, no additional insertion loss due to the difference of resonance characteristics is caused and, as a result, isolation characteristics can be improved as described above.

[0083] ———Moreover, since the phase adjustment element 9 is connected to the reception side surface acoustic wave filter 6, the DPX coupling loss on the side of the common terminal 4 on the antenna side can be reduced.

[0084] ———In the present preferred embodiment, ~~preferably~~, the amount of phase rotation by the phase adjustment element 9 of the reception side surface acoustic wave filter 6 is preferably made less than about 90 degrees from the center frequency of the passband of the reception side surface acoustic wave filter. In this case, since the amount of phase rotation can be made smaller, the phase adjustment element can be reduced in size and, as a result, the surface acoustic wave branching filter 1 can be ~~downsized~~ reduced in size.

[0085] ———In particular, when the amount of phase rotation is made less than about 90 degrees, in a stage before the transmission side surface acoustic wave filter 5 and the reception side surface acoustic wave filter 6 are coupled on the antenna side, the phase is made inductive in the passband of the reception side surface acoustic wave filter 6 and the phase is made capacitive in the passband of the transmission side surface acoustic wave filter 5. Thus, ~~the~~ impedance matching can be realized. ~~In particular~~ As shown in Fig. 11, in the construction in which the resonator ~~the~~ that is closest

to the common terminal 4 on the antenna side is a series-arm resonator, ~~when~~ the passband of the transmission side surface acoustic wave filter 5 is made capacitive, ~~as shown in Fig. 11,~~ ~~the larger~~ the capacitance, ~~the larger~~ and the movement on the Smith chart become larger and, thus, the reflection increases. Accordingly, the loss at the DPX coupling increases.

[0086] — On the contrary, in the case ~~in which, as in the~~ present preferred embodiment, a resonator ~~the that is~~ closest to the common terminal 4 on the antenna side is the parallel-arm resonator T1, ~~when.~~ When the passband of the transmission side surface acoustic wave filter is made capacitive by addition of the parallel-arm resonator T1, ~~since~~ the movement as shown in Fig. 10 is performed, ~~the.~~ The reflection decreases and, as a result, deterioration of characteristics at the DPX coupling can be ~~suppressed~~ reduced.